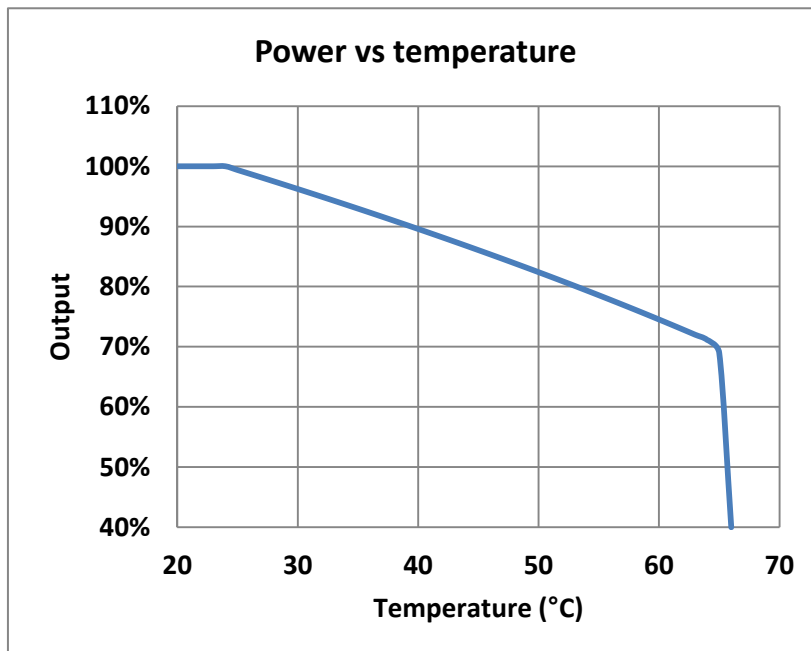


## Technical notes on output rating, operating temperature and efficiency

### 1. Inverters: continuous output rating as function of temperature

In our datasheets inverters, and the inverter function of Multis and Quattros, are rated at 25°C (75°F). On average, derating at higher temperatures is as shown below (see paragraph 4 for the theoretical background).

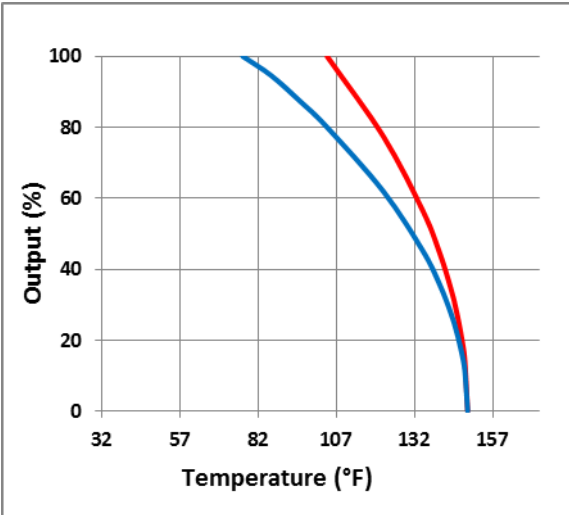
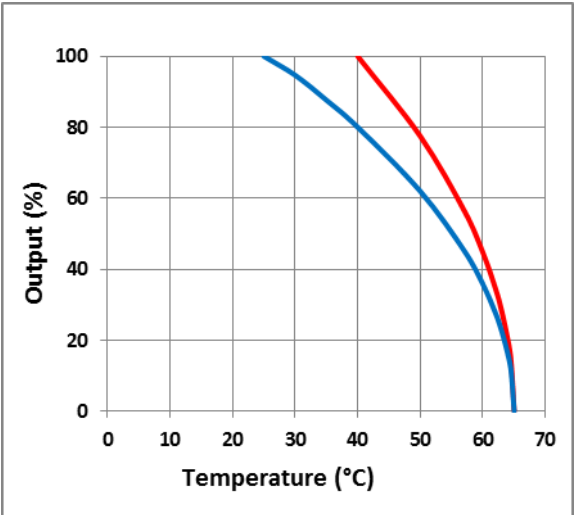
Temperature		Cont. output
°C	°F	%
Low temp.		100
25	77	100
30	86	96
35	95	93
40	104	90
50	122	82
60	140	75
65	149	69
High temp.		0



## 2. Battery chargers: continuous output rating as a function of temperature

In our datasheets battery chargers are rated at 40°C (104°F). The battery charger function of our Multis and Quattros is rated at 25°C (77°F). As explained in paragraph 4, derating for higher temperatures is approximately as follows:

Blue curve: products rated at 25°C (77°F)			Red curve: products rated at 40°C (104°F)		
Temperature		Cont. output	Temperature		Cont. output
°C	°F	%	°C	°F	%
25	77	100			
30	86	95			
35	95	88			
40	104	80	40	104	100
50	122	62	50	122	77
60	140	36	60	140	45
65	149	0	65	149	0

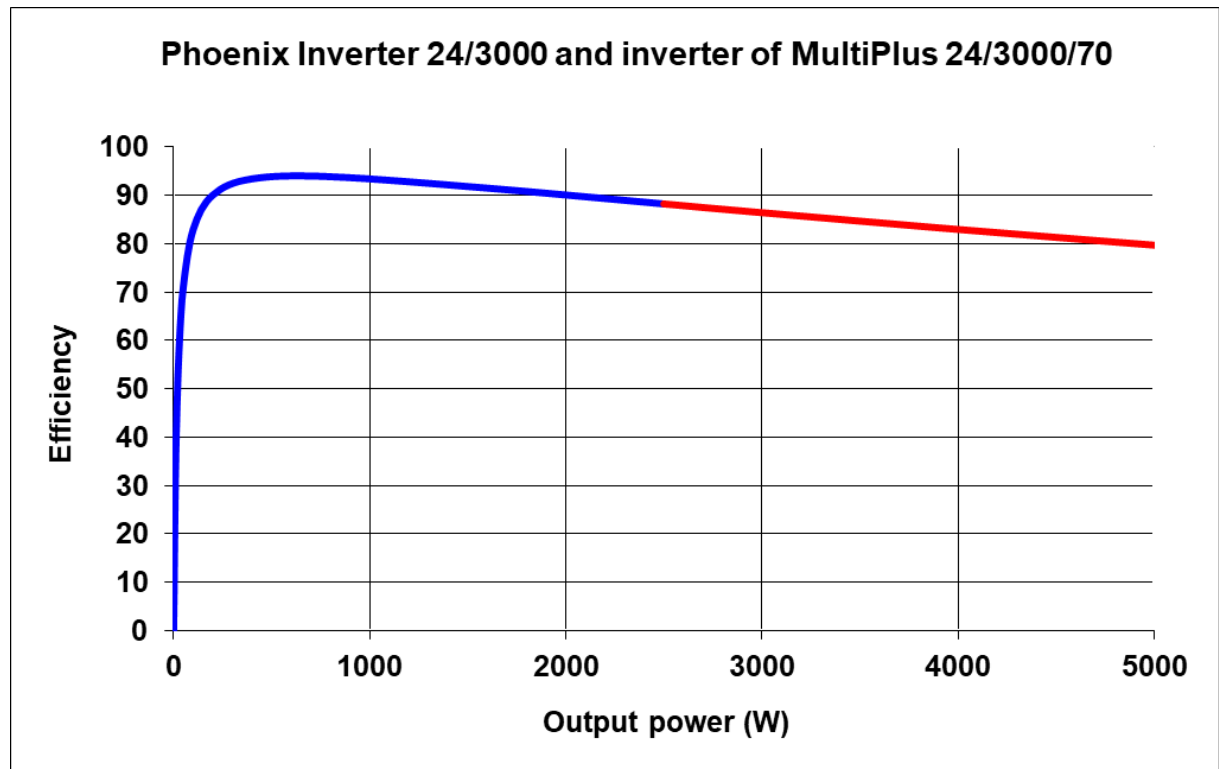


### 3. Power loss and efficiency as a function of load

As an example let us look at the Phoenix Inverter 24/3000 or MultiPlus 24/3000/70 (both products have the same inverter). These products use high frequency switching to generate a sinewave, which is then transformed to the required output voltage by two toroidal transformers. Toroidal transformers have a higher efficiency and less no load losses than the more common E-core transformers.

The measured efficiency curve is shown below:

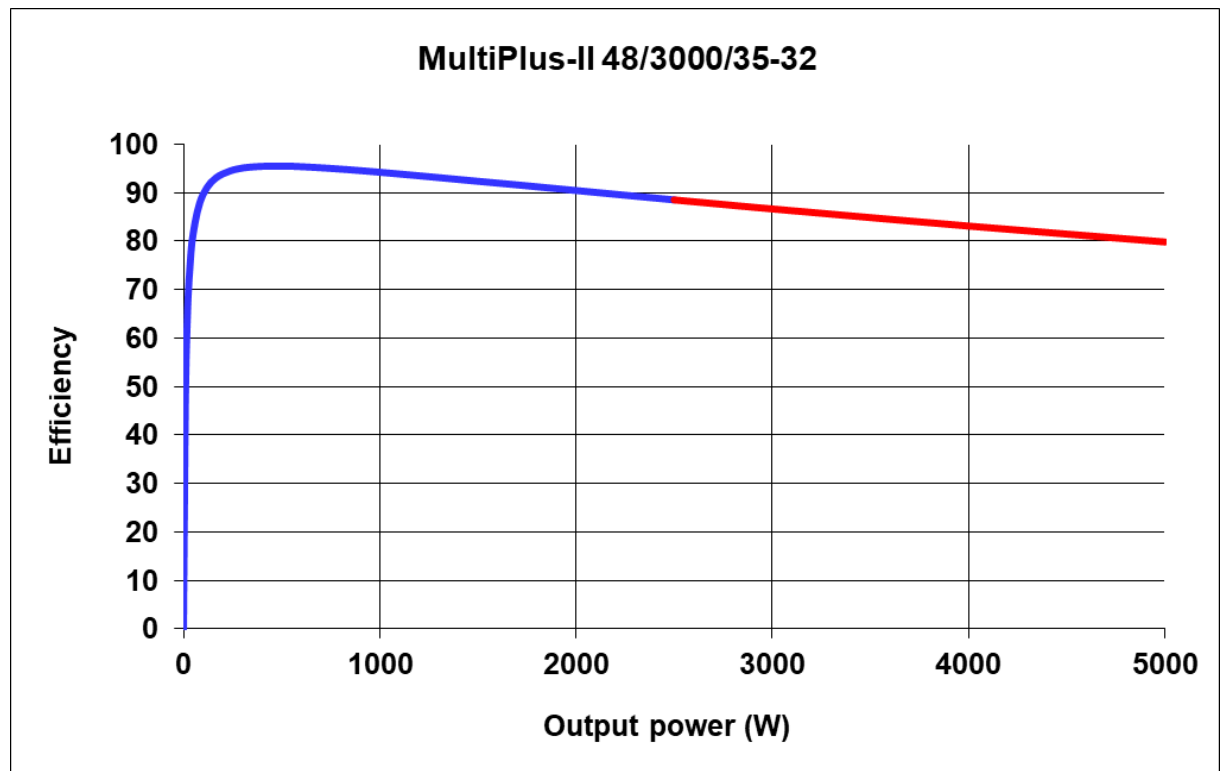
Output power (W)	Dissipation (W)	Efficiency (%)
0	20	0
10	20	33,3
20	20	50,0
30	20	59,9
50	20	71,3
100	21	83,0
200	22	90,1
400	28	93,5
800	52	93,9
1600	148	91,5
2500	333	88,3
3000	470	86,5
4000	820	83,0
5000	1270	79,7



Recently a new product has been introduced: the MultiPlus-II 48/3000/35-32  
(this is exactly the same product as the MultiGrid-II 48/3000/35-32)

The MultiPlus-II has only one toroidal transformer, and several other improvements to reduce no load power consumption. As can be seen from the table and graph below, this product is more efficient, especially at low load.

Output power (W)	Dissipation (W)	Efficiency (%)
0	11	0
10	11	47,6
20	11	64,5
30	11	73,1
50	11	81,8
100	12	89,7
200	13	93,9
400	19	95,5
800	43	94,9
1600	139	92,0
2500	324	88,5
3000	461	86,7
4000	811	83,1
5000	1261	79,9



## 4. The theory behind the graphs of paragraph 1 – 3

### 4.1. Operating temperature range

The operating temperature range may vary from one product to another.

The upper temperature is limited by the maximum operating temperature of certain components (for ex. semiconductors, electrolytic capacitors, relays).

The low temperature limit is mainly limited by the minimum operating temperature of semiconductors and electrolytic capacitors.

As has been shown in section 1 and 2, this does not mean that the full output rating is available over the whole temperature range.

Derating is needed at high ambient temperatures to prevent overheating of a.o. power semiconductors and transformers.

In general, output power cannot be increased at low temperatures due the maximum current rating of certain components (terminals, core saturation of filter chokes).

### 4.2. Power loss and efficiency

Electric current generates heat in the conductor through which it flows. The basic formula to calculate the rate of heat generation, or power dissipation, is:

$$P = R \times I^2 \quad (1)$$

where P stands for power (measured in Watts), R (Ohm) is the resistance of the conductor and I (Ampère, or Amps) the current.

What is interesting about this formula is that it shows that power dissipation increases with the square of the current. A resistance of for example 2 Ohm and a current of 10 Amps results in a dissipation of  $2 \times 10 \times 10 = 200$  W. Twice that current results in 4 times more heat generated:  $2 \times 20 \times 20 = 800$  W!

In power electronic circuits the situation is much more complicated: one has to do with DC losses and switching losses, losses in semiconductors and in high frequency transformers, etc. Very often, however, formula (1) appears to be a fairly good approximation of the overall losses in the circuit. The power dissipation P of the circuit can then be calculated by defining R as the overall resistance between input and output of the circuit and I as the output current.

An even better approximation is obtained if a factor is added to (1) to account for the no-load power consumption or no-load power dissipation. The no-load power consumption is the power dissipated by the circuit when it is switched on without any load connected. It is an important specification especially of inverters since in the long run it can drain a battery.

Taking into account the no-load power consumption results in the following formula:

$$P_{\text{loss}} = P_0 + R \times I_{\text{out}}^2 \quad (2)$$

$P_{\text{loss}}$  is the total power dissipation in the product;  $P_0$  is the no-load power dissipation (and by definition also the no-load power consumption); R is the "resistance" between input and output; and  $I_{\text{out}}$  the output current.

With formula (2) efficiency, an important specification of inverters, can be calculated:

$$\eta = 100 \times P_{\text{out}} / (P_{\text{out}} + P_{\text{loss}}) \quad (3)$$

where  $\eta$  is the efficiency in % and  $P_{\text{out}}$  the output power ( $P_{\text{out}} = V_{\text{out}} \times I_{\text{out}}$ ).

At no-load conditions the output current  $I_{out} = 0$  and the output power  $P_{out} = 0$ , so that:

$$P_{loss} = P_o \quad (4)$$

and:

$$\eta = 0 / (0 + P_o) = 0 \% \quad (5)$$

In other words: the efficiency is 0 at no-load.

If there would be no power dissipation in the circuit ( $P_{loss} = 0$ ), then:

$$\eta = 100 \times P_{out} / (P_{out} + 0) = 100 \% \quad (6)$$

In words: if an ideal circuit without any losses could be made, efficiency would be 100 %.

Formula (2) shows that with increasing load the losses at first do not increase very quickly because  $P_o$  will still be very much larger than  $R \times I_{out}^2$  as long as  $I_{out}$  is small. Efficiency will start at 0 and increase when the load increases.

But with the load increasing further,  $R \times I_{out}^2$  will increase even faster and become larger than  $P_o$ , so that  $P_{loss}$  will start increasing approximately with the square of the load or output current. After reaching a maximum, efficiency will therefore start decreasing as the load increases further.

#### **4.3. High temperature and derating**

All power conversion products of Victron Energy are protected against damage due to overheating by temperature sensors placed on transformers and on the heatsink of the hottest semiconductors.

**Inverters:** When the power semiconductors and / or transformers reach a pre-set temperature, inverters will first show a temperature pre-warning, and if temperature increases further, the inverter will shut down. After cooling down, it will restart.

**Battery chargers:** When the power semiconductors and / or transformers reach a pre-set temperature, the output current will automatically be reduced to prevent a further increase in temperature.

The power semiconductors are the most critical, with a pre-set maximum heatsink temperature of approximately 80°C (167°F).

High frequency magnetics are in general limited to 100°C, and toroidal transformers to 110°C.

The derating curve resulting from maximum heatsink temperature will therefore show a steeper downward slope than the derating curve resulting from high frequency magnetics or a toroidal transformer.

In general the toroidal transformer is the limiting factor in our inverters and inverter/chargers, while semiconductors are the limiting factor in our battery chargers. This explains the difference between the curves shown in paragraph 1 and paragraph 2.

Knowing that, in case of forced cooling, the cooling capacity of a heatsink or transformer is proportional to the temperature difference between the heatsink/transformer and the cooling air flow, formula (2) can be restated as follows:

$$I_{out} = K \times \sqrt{(T_{max} - \Delta T_o - T_{amb})} \quad (7)$$

where  $I_{out}$  is the output current;  $K$  is a constant;  $T_{max}$  is the maximum heatsink or transformer temperature;  $\Delta T_o$  is the temperature rise of the heatsink or transformer due to the no-load power dissipation; and  $T_{amb}$  is the temperature of the cooling air flow.

Formula (7) shows that when  $\Delta T_o + T_{amb} = T_{max}$ ,  $I_{out} = 0$ .

In words: when the ambient temperature is so high that the no load power dissipation alone will cause the heatsink or transformer to reach the maximum temperature limit, the output current of the circuit is 0. Any output current would increase temperature beyond the maximum and result in shut down of the circuit due to overheating.

The derating formula (7) is applicable when the ambient temperature increases beyond the temperature at which the full output power is specified, in general 25°C (77°F) for inverters and 40°C (104°F) for battery chargers.

Why 25°C (77°F) for inverters? Inverters are very often used with intermittent loads. Short term power and peak power are therefore more important than the continuous rated power. Battery chargers on the contrary will regularly operate at maximum output current for several hours and are therefore rated for continuous operation at 40°C (104°F).